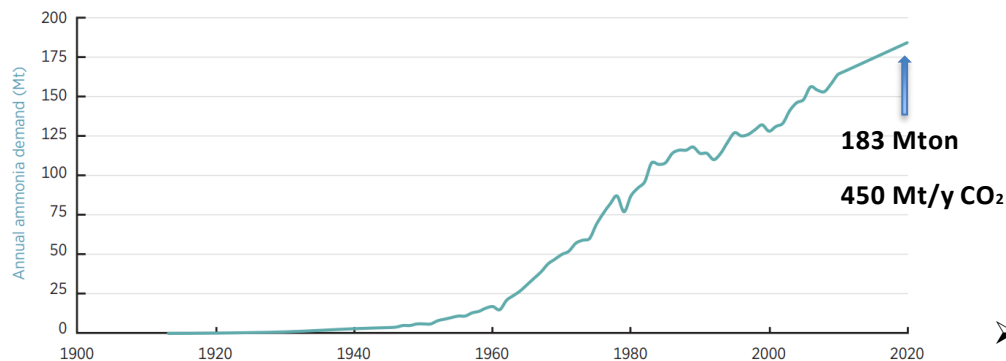


## Unlocking the potential of ammonia as energy vector in energy transition: Market Trends and techno-economic assessment of ARENHA solutions



*The present publication reflects only the author's views. The Commission is not responsible for any use that may be made of the information contained therein.*

## Ammonia Demand and Applications

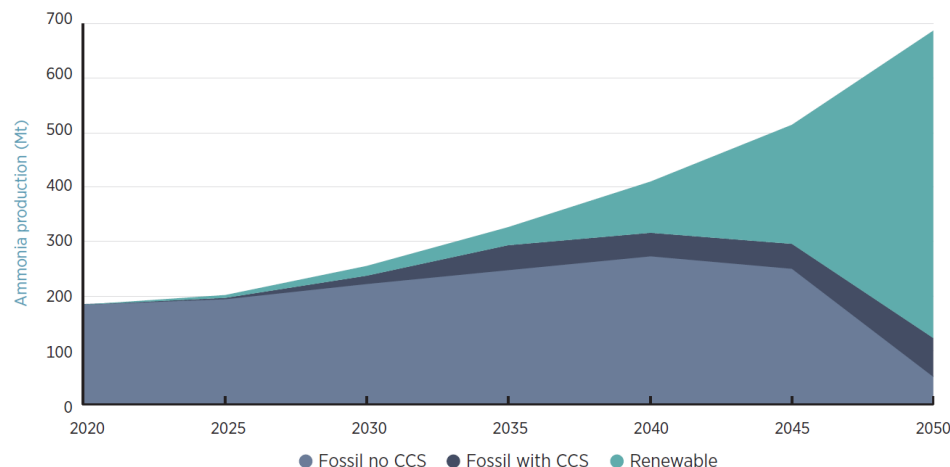


Global Ammonia demand (1900-2020) Source: Innovation Outlook, Renewable ammonia; IRENA 2024

Hydrogen sourcing for  $\text{NH}_3$  synthesis reaction:

- Gas Reforming
  - Coal Gasification
  - Gas Reforming with CCS
  - Water Electrolysis
- 1.8-3.2  $\text{tonCO}_2/\text{tonNH}_3$   $\text{CO}_2$
- Low-Carbon Ammonia

➤  $\text{NH}_3$  demand could reach more than three times 2020 demand by 2050



Innovation Outlook, Renewable ammonia; IRENA 2024

### Existing uses:



Fertilizers (~80%)



Plastics



Textiles



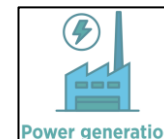
Explosives



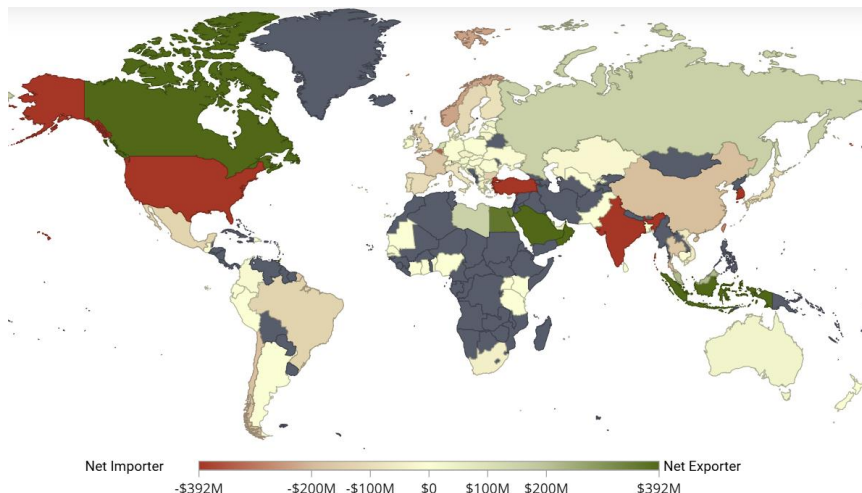
Refrigeration

- The industry's current path is incompatible with climate neutrality goals.
- Low-Carbon ammonia** could play a broader role in the energy transition, contributing to the **decarbonization** of the **chemical industry**, **transportation** and **power generation** sectors.

New Emerging uses:



## Ammonia Market Trade



*Anhydrous ammonia Product trade, Exporters and Importers in 2023  
| Source: Observatory of Economic Complexity*

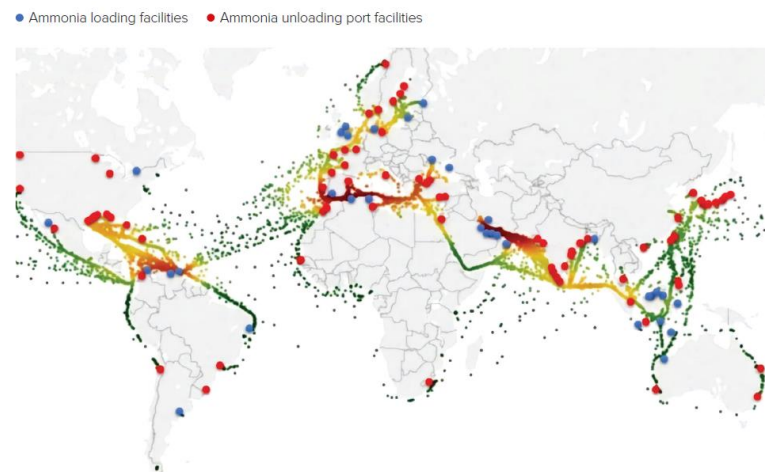
### Main Exporters:

- Trinidad and Tobago (18.6%), Saudi Arabia (15.3%), Indonesia (10%) and Canada (8.85%)

### Main Importers:

- US (15.2%), India (13.6%), Morocco (9.75%), Turkey (4.81%) and Cina (3.51%)

- In 2023 **15 Mton** of NH<sub>3</sub> were traded worldwide, for a total market value of **9 Bn\$**

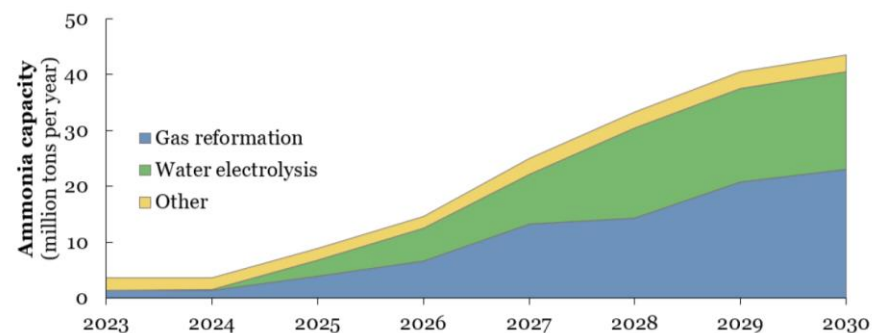


*Ammonia shipping infrastructure in 2017 , including a heat map of liquid ammonia carriers and existing ammonia port facilities. | Source: The Royal Society*

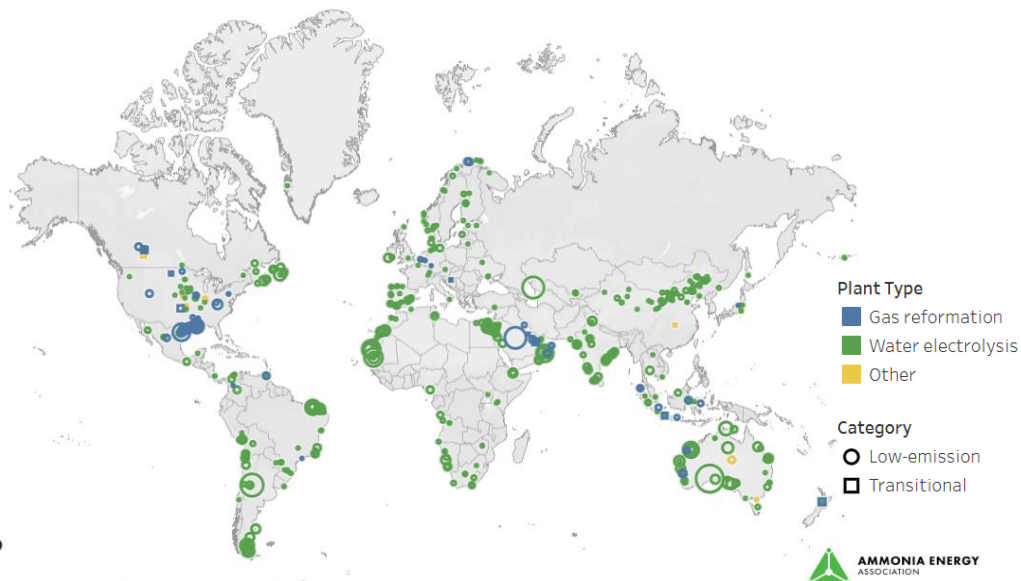
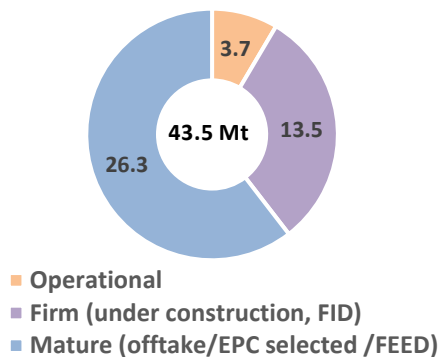
**Existing ammonia trading infrastructure can support low-carbon ammonia exports**

## Low-Carbon Ammonia Supply

- **485** Ammonia projects (Feb. 2025) from 102 (Dec. 2022) for a total **451.2** millions tons (Mt)
- 43.5 Mt ammonia capacity could be operational by 2030, **37.7 Mt** low-carbon (~90%)



Operational, firm and mature Low-carbon ammonia projects. | Source: Ammonia Energy Association



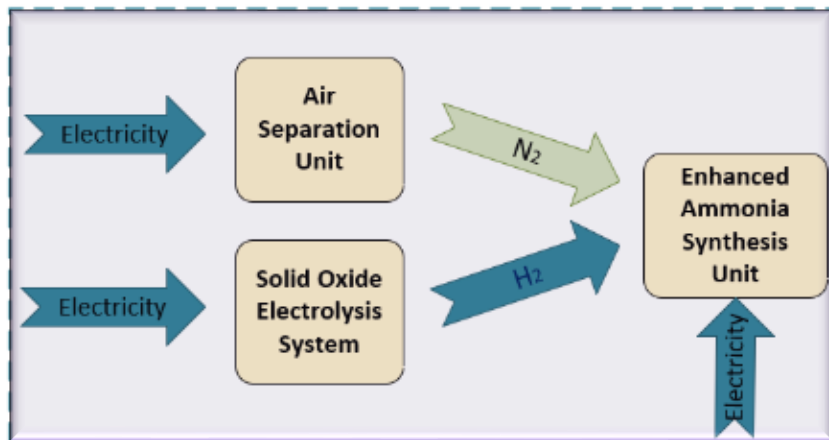
Announced ammonia projects. | Source: Ammonia Energy Association

- Low-carbon ammonia project based on natural gas (blue) set to lead near term supply compared to electrolysis based (green) ammonia projects
- High financing cost and low offtakers willingness to pay is a barrier for green ammonia project developments

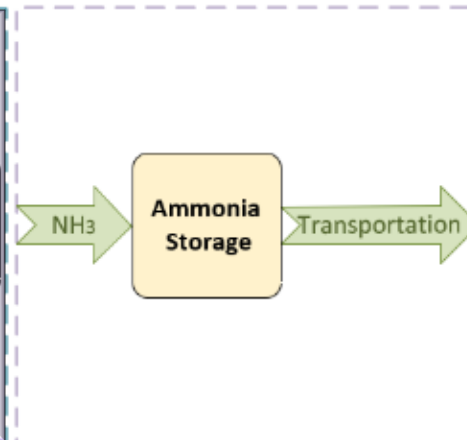
Need of **affordable** and **cost effective** green ammonia production technologies to move more projects towards Final Investment Decision (FID)

## ARENHA Techno-economic Assessment

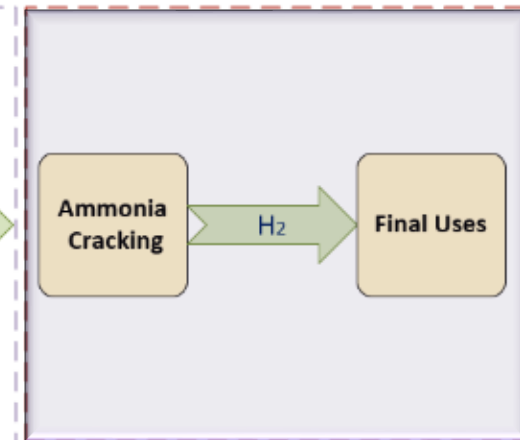
### 1. Power-to-Ammonia



### 2. Ammonia Storage



### 3. Ammonia-to-Power



### Objectives:

- Technology benchmarking;
- Optimize system design and evaluate economic feasibility;
- Gain valuable technical insights to help make investment decision;

### Solutions modelled:

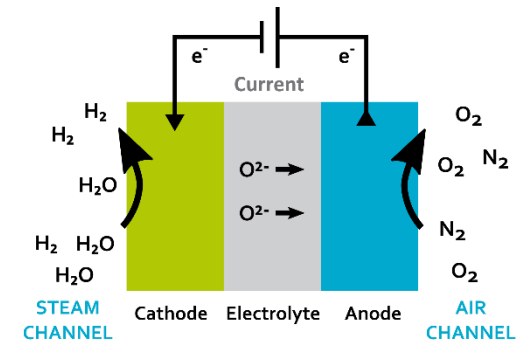
- Power-to-Ammonia
- Ammonia Solid Storage
- Ammonia-to-Hydrogen

## Why Solid Oxide Electrolysis Cells (SOECs)?

Cathode semi-reaction:  $H_2O + 2e^- \rightarrow H_2 + O^{2-}$

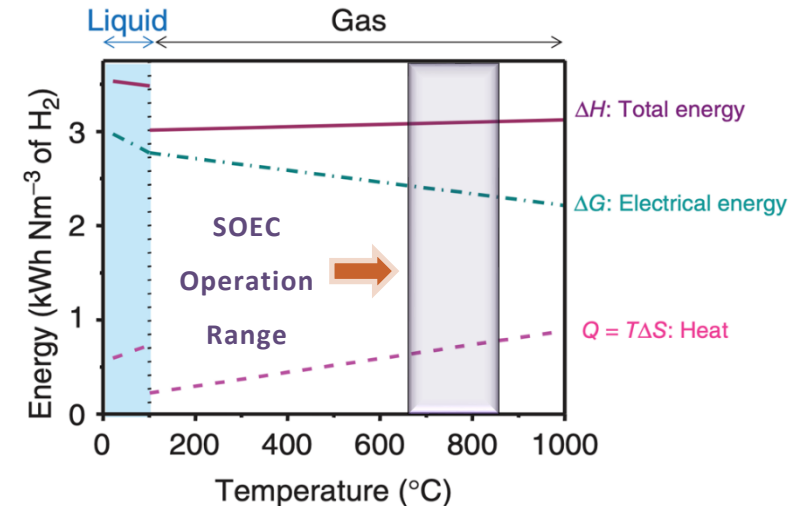
Anode semi-reaction:  $O^{2-} \rightarrow \frac{1}{2}O_2 + 2e^-$

Overall Reaction:  $H_2O \rightarrow \frac{1}{2}O_2 + H_2$



### Key Advantages of high temperature operation :

- Lower total and electrical energy expenditure → Higher efficiency (Lower OPEX)
- No need for Platinum-Group Metals (PGMs) → More robust supply chain
- Heat integration possibility (e.g. Power-to-X applications)



Energy need for the water electrolysis reaction, as function of temperature, enthalpy ( $\Delta H$ ), Gibbs free energy ( $\Delta G$ ) and entropy ( $T\Delta S$ ) (Source: G. Jopek, "Hydrogen Production by Electrolysis", 2018)

## Solid Oxide Electrolysis Process Overview

High-temperature electrolysis process steps:

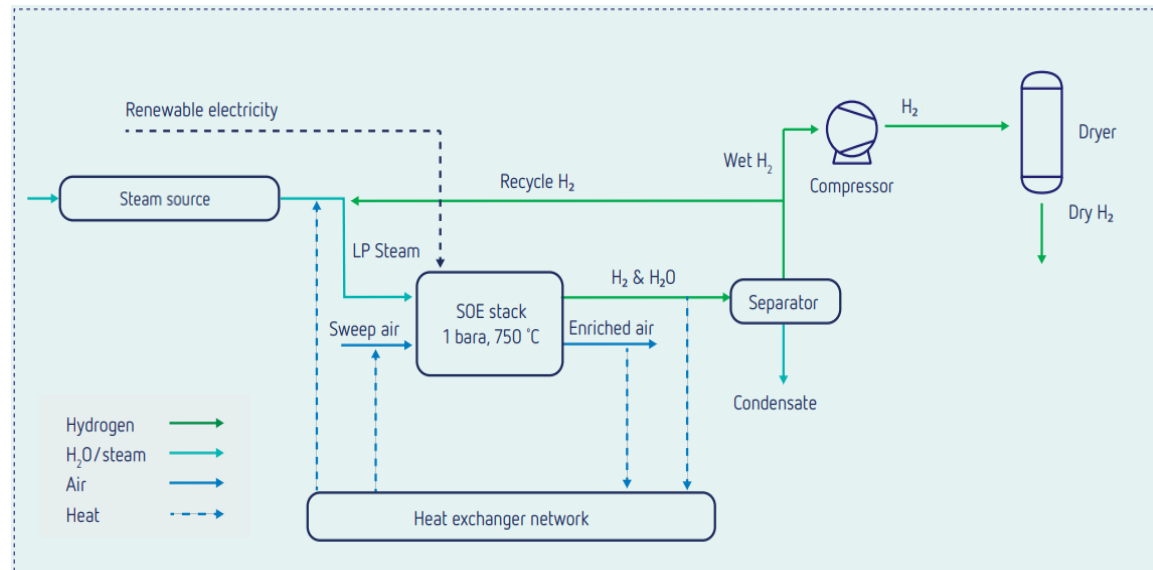
1. Steam Generation

2. Cathodic/anodic streams pre-heating

3. Electrolysis

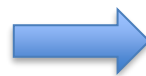
4. Water Separation

5. H<sub>2</sub> Compression & Drying



Green Hydrogen Production Process Based on SOEC (Source: ISPT, "Next Level Solid Oxide Electrolysis", 2023)

**~5 kW ARENHA pilot!** How to scale-up system for industrial application?



- Cell/stack development and scale-up
- Modular system approach



### Solid Oxide Electrolysis Process: Modularity

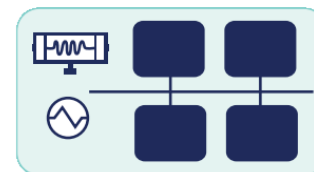
1. SOEC Cell (~W)



2. SOEC Stack (~kW)

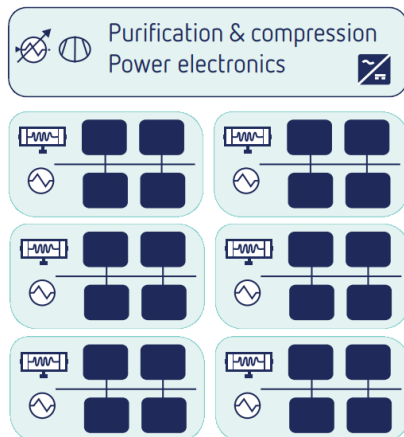


3. SOE Stack Module (Hot-box) (~kW to MW)

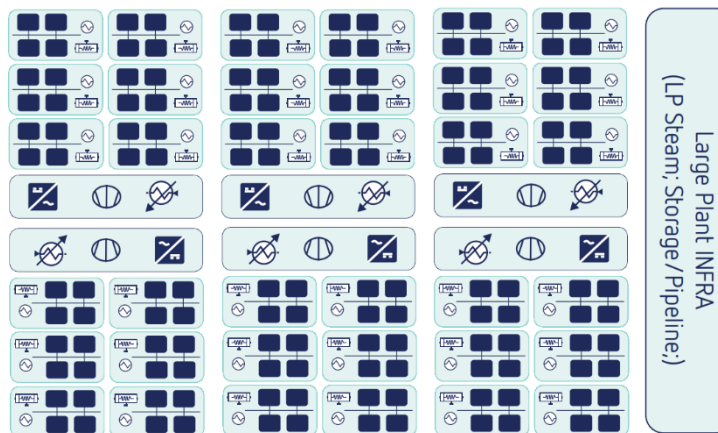


4. SOE System

Repeating Block (~MW)



5. Complete SOE Plant (~MW)



**World biggest SOE project:**

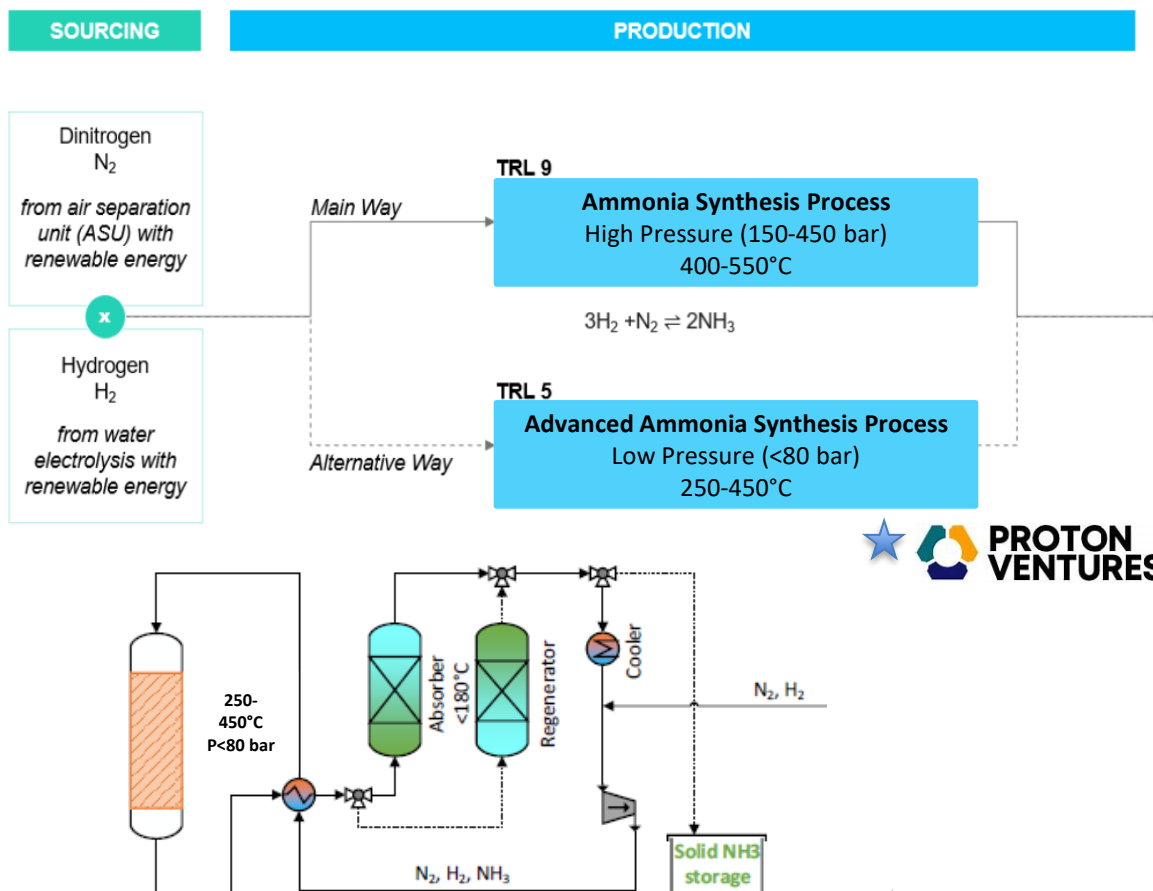
Mountain view NASA  
Facility (Bloom Energy):  
4 MW<sub>DC</sub> (~2.4 tH<sub>2</sub>/d)





## ARENHA Ammonia Synthesis Process

- **Advanced ammonia synthesis process** developed in ARENHA consists of **ammonia separation** using **absorption** process allowing for **milder operating conditions**



### Advantages of ARENHA advanced ammonia synthesis technology:

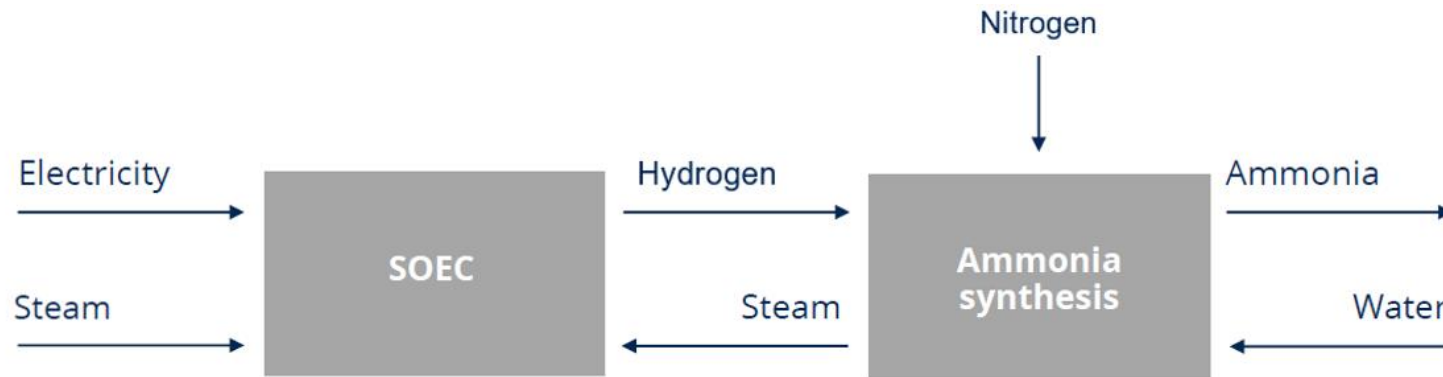
- **Lower equipment cost (15-20%)**
- **Energy consumption comparable** to traditional small scale green ammonia synthesis technologies;
- **No CO<sub>2</sub> emissions;**
- **High system flexibility** enhanced by milder operating conditions.



★ **Patented solution**

## ARENHA Power-to-Ammonia

### Synergy between Solid Oxide Electrolysis and Ammonia synthesis processes



#### – Solid Oxide Electrolyser (SOE)

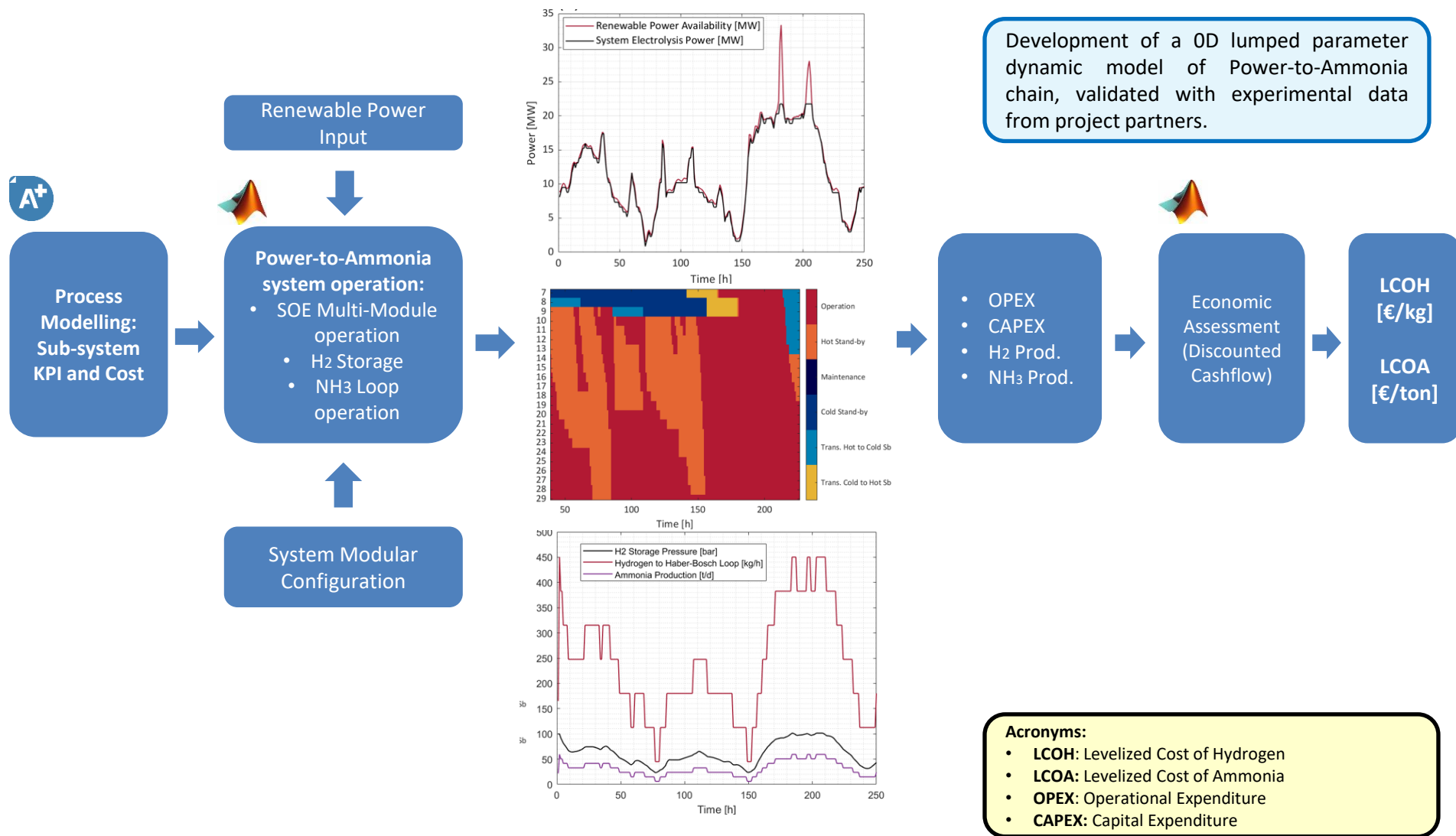
- Lower energy consumption for H<sub>2</sub> production (47-50 kWh/kg<sub>H2</sub>) compared to low temperature electrolysis solutions;
- High energy demand for steam vaporization (~ 20 % of total electrolyser electricity consumption):

#### – Ammonia Synthesis Loop

- High quality heat availability (T > 400°C) from ammonia synthesis reaction which can be used for steam production.

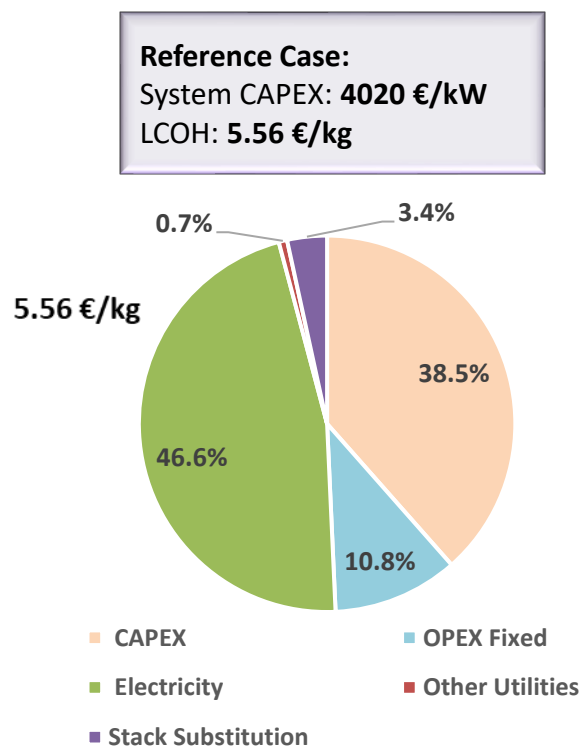
The **integration** of steam produced in ammonia synthesis loop in Solid Oxide Electrolyzer enables for superior efficiency, offering **greater performances** and **cost reduction potential** compared to low-temperature electrolysis-based Power-to-Ammonia solutions.

### Techno-economic Assessment Methodology

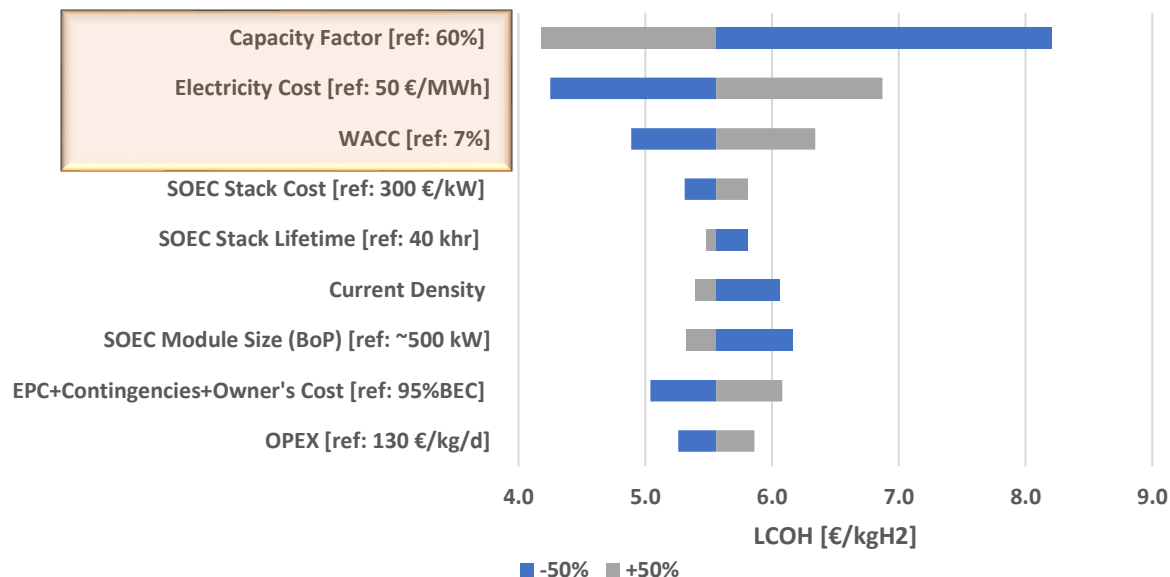


## Results: Solid Oxide Electrolysis

~16 MW electrolysis power system (11.15 t/d H<sub>2</sub>) fed by PV/Wind hybrid system



60% system availability. 30 Year plant operation, 50€/MWh electricity cost, 7% discount rate. Hydrogen output : 30 bar.



### Acronyms:

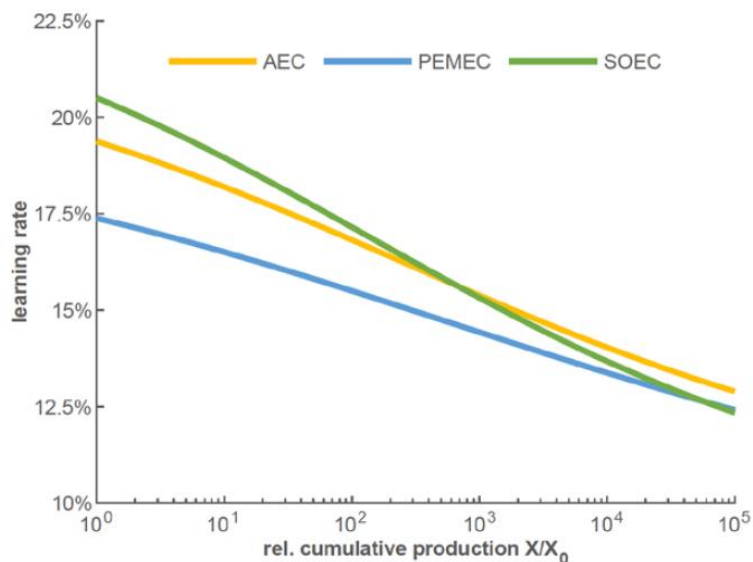
**LCOH:** levelized Cost of Hydrogen | **BEC:** Bare Erected Cost | **BoP:** Balance of plant |  
**WACC:** Weighted average cost of capital | **EPC:** Engineering Procurement and construction

### OPEX and CAPEX driven process. Main cost affecting parameters:

- Renewable energy availability (Capacity Factor);
- Electricity Cost;
- Project financing cost;

## Results: Solid Oxide Electrolysis

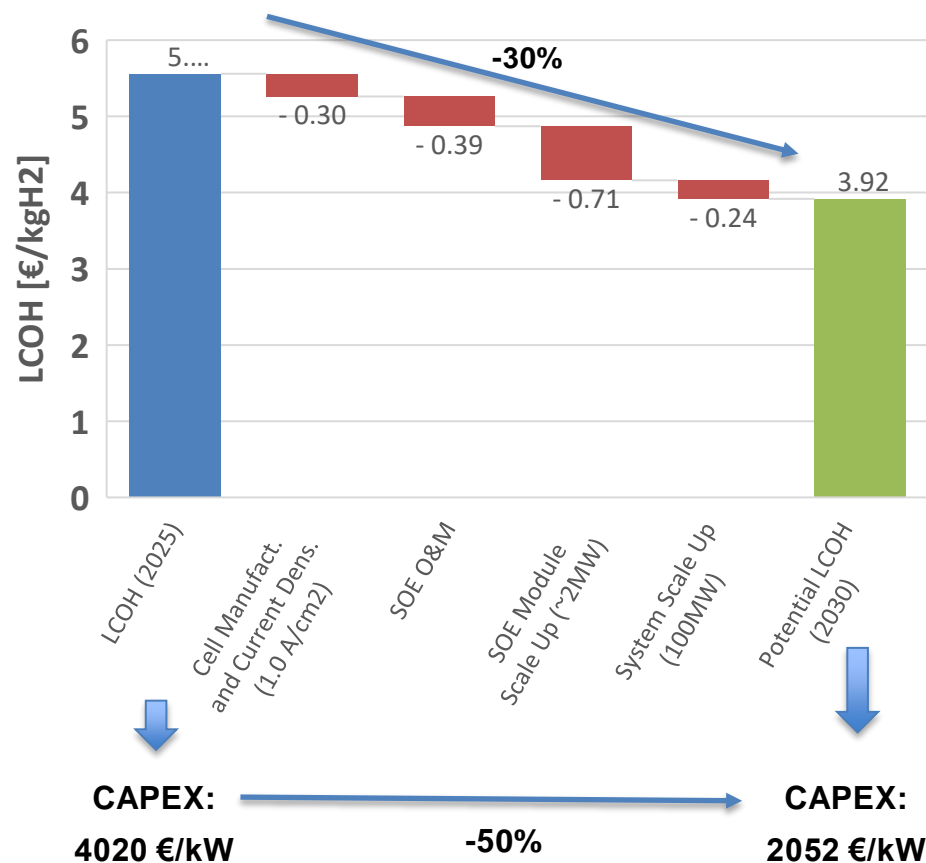
### Potential LCOH reduction driven technology improvement and CAPEX reduction



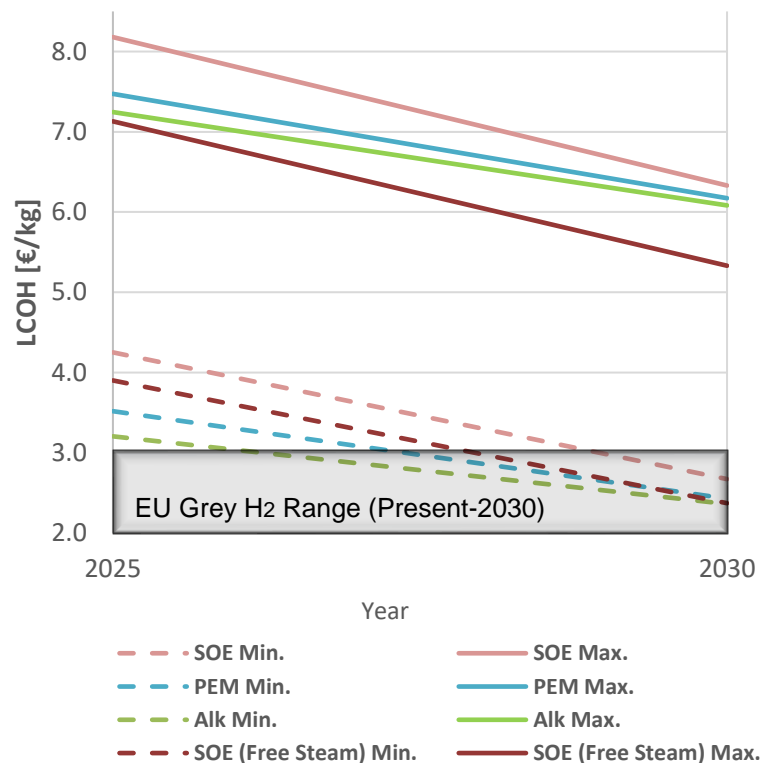
Estimated Learning rate of main electrolysis technologies.  
(Source: IRENA)

- Solid Oxide Electrolysis benefit of a higher cost potential reduction (learning rate) compared to low temperature electrolysis technologies

**Technology improvement, higher manufacturing rate and system scale up are crucial for CAPEX and LCOH reduction in SOE systems**



### Results: Solid Oxide Electrolysis vs Low-T Electrolysis Technologies



Electrolyzers operated with 60% year average capacity factor. Min and Max. refer respectively to 25 and 100 €/MWh electricity cost scenario. 30 years plant lifetime and 7% discount rate assumed. PEM and Alk. CAPEX and stack cost from STEPS scenario in [2]. 2025 PEM system energy consumption from [3], 2025 Alkaline system energy consumption from [4]. 2030 System energy consumption scenarios from [1].

- [1]. [Clean Hydrogen JU - SRIA Key Performance Indicators \(KPIs\) - Clean Hydrogen Partnership](#)
- [2]. IEA, Global Hydrogen Review, 2024
- [3]. Cummins Hylizer specsheet, 2021
- [4]. Sunfire-Hylink Alkaline specsheet, 2025

Scenario	2025				2030			
Electrolysis Technology	Alk	PEM	SOE	SOE (free steam)	Alk	PEM	SOE	SOE (free steam)
Installed Electrolysis Power [MW]	24.2	23.7	15.9	15.9	140	140	100	100
Hydrogen Production [t/d]	11.15				70.00			
Tot. CAPEX* [€/kW] [2]	2000	2450	4020	3921	1250	1400	2052	1980
System Energy Consumption [kWh/kg <sub>H2</sub> ]	52	51	49.85	41.10	48	48	47.85	39.10

\*CAPEX is calculated per kW of installed electrolysis power.

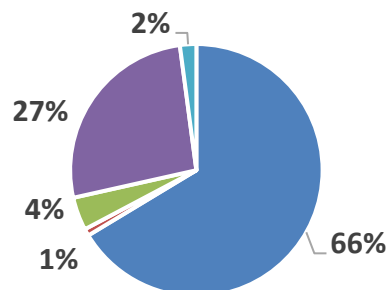
**O&M:** Operation and Maintenance | **Alk:** Alkaline electrolyser | **PEM:** Proton exchange membrane electrolyzer | **SOE:** Solid Oxide Electrolyzer

**Despite higher cost greater efficiency makes SOE potentially competitive with low-T electrolysis technologies, especially for high electricity cost and free steam to electrolyzer scenarios**

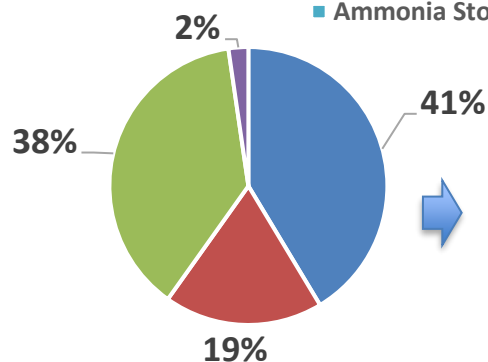
## Results: Power-to-Ammonia

Power-to-Ammonia system based on SOE - ~16MW electrolysis power (~60t/dNH<sub>3</sub>):

**Reference Case:**  
System CAPEX: ~100 M€  
LCOA: 1483 €/tonNH<sub>3</sub>



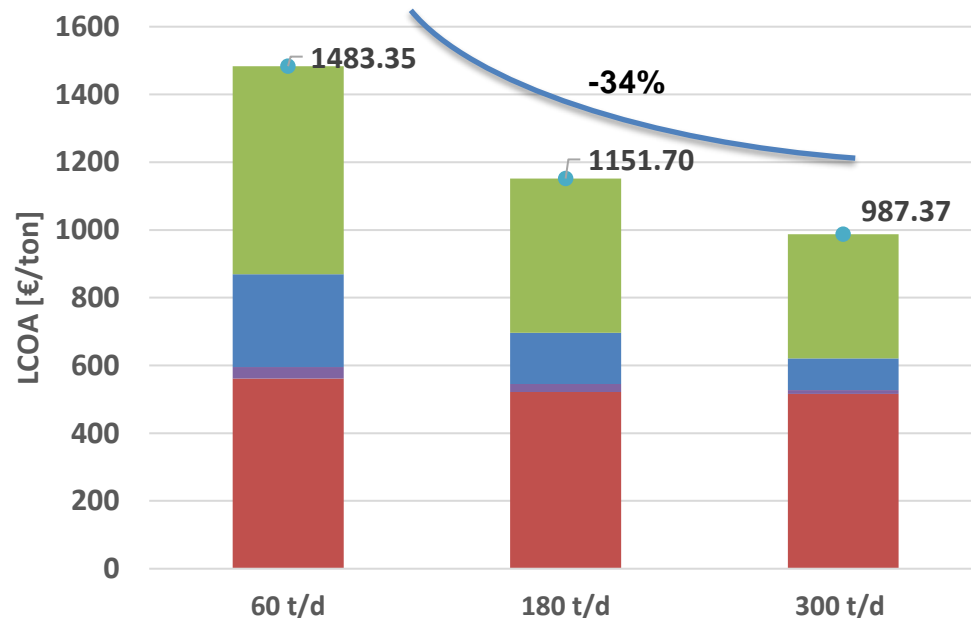
■ Hydrogen Production ■ Hydrogen Storage  
■ Nitrogen Production ■ Ammonia Production  
■ Ammonia Storage



System economic is challenged at 60 t/d scale with CAPEX and O&M representing two third of total LCOA

■ CAPEX ■ OPEX  
■ Energy & utilities ■ Stack Substitution

Improving economics with system scale:



■ Energy & utilities ■ Stack Substitution ■ O&M ■ CAPEX

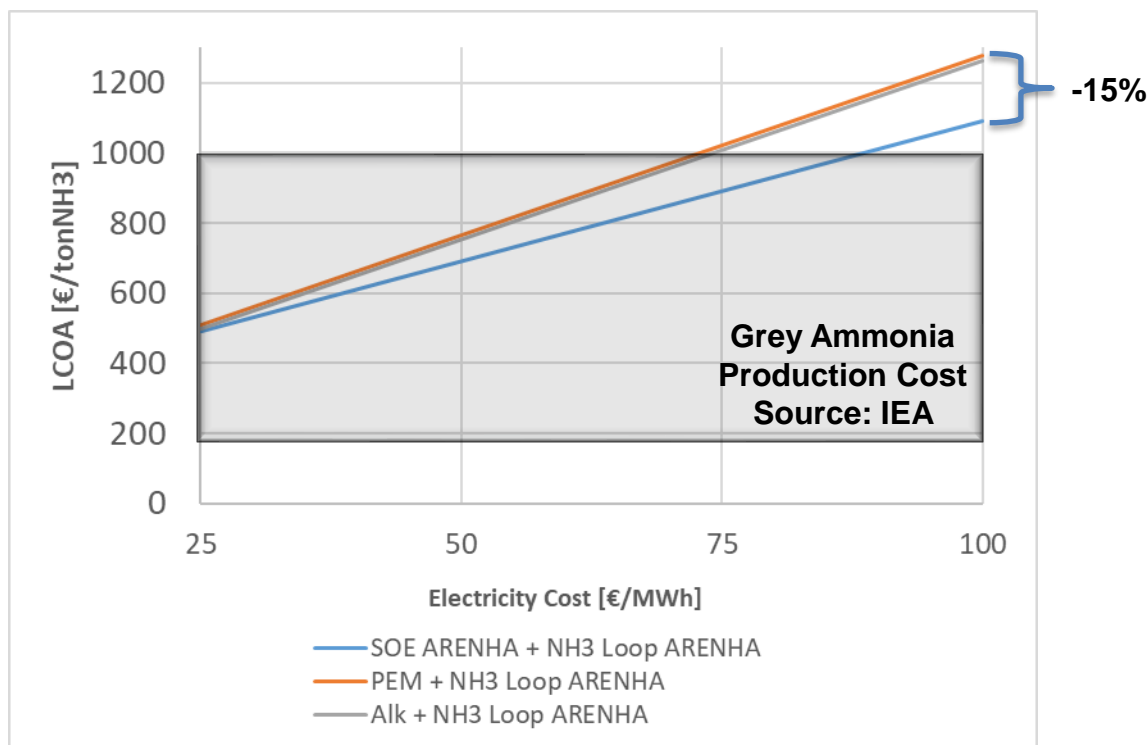
System operated with 60% year average capacity factor. 50€/MWh electricity cost, 30 years plant lifetime and 7% WACC assumed. A 100 bar H<sub>2</sub> storage, 30 days ammonia storage and Nitrogen production were included in the study.

**Increasing system scale could allow for economic competitiveness with traditional production pathways**



## Results: Power-to-Ammonia

### Comparison with low-temperature based PtA system



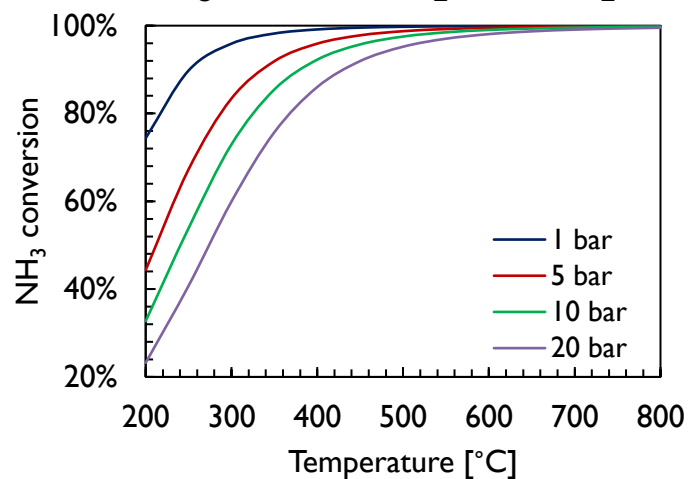
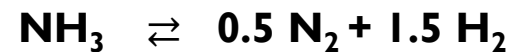
Analysis carried out for ~300 tNH<sub>3</sub>/d Power-to-Ammonia based on SOE, Alkaline and PEM electrolysis technologies, 90% system availability, 30 years plant lifetime and 7% discount rate.

ARENHA Power-to-Ammonia solution based on SOE could be competitive with Power-to-Ammonia solutions based on low temperature electrolysis technologies and with traditional production (in case favourable electricity market conditions)

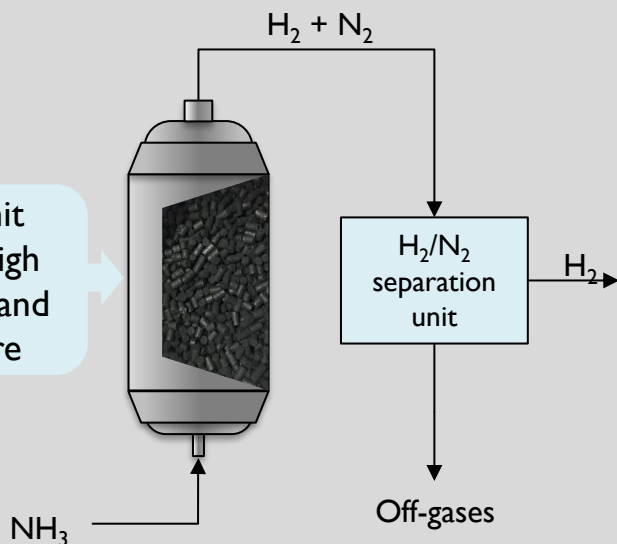


### What is required

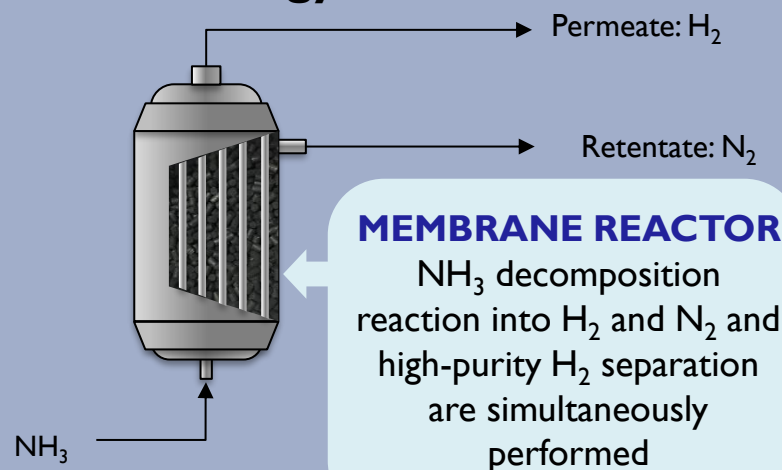
- Continue R&D activities on SOE and enhanced NH<sub>3</sub> Synthesis
- Effort in scaling up (e.g. SOE stacks and modules)
- High energy utilisation and low electricity cost from renewable energy assets

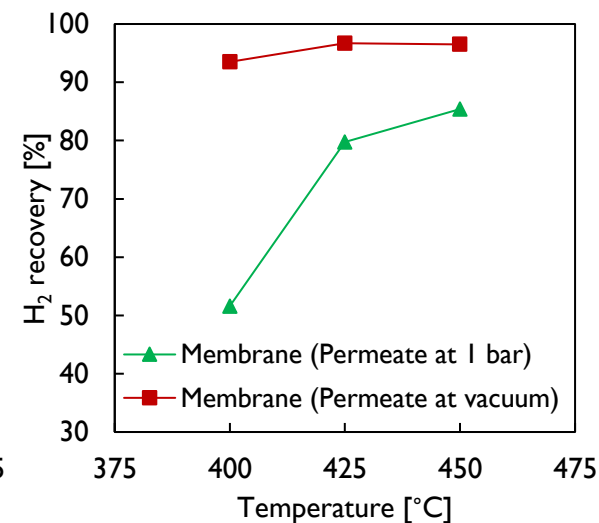
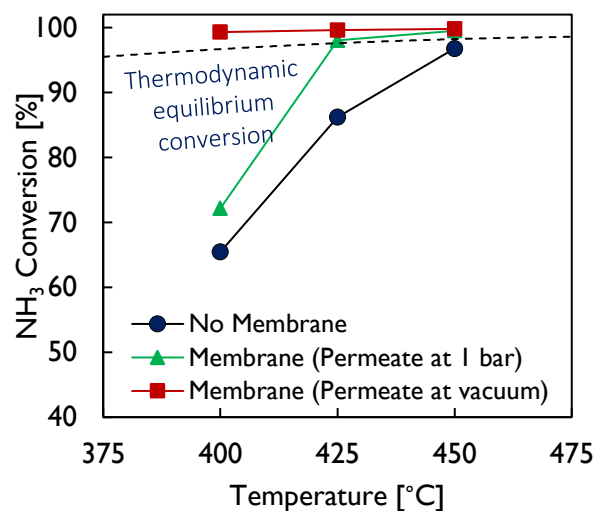
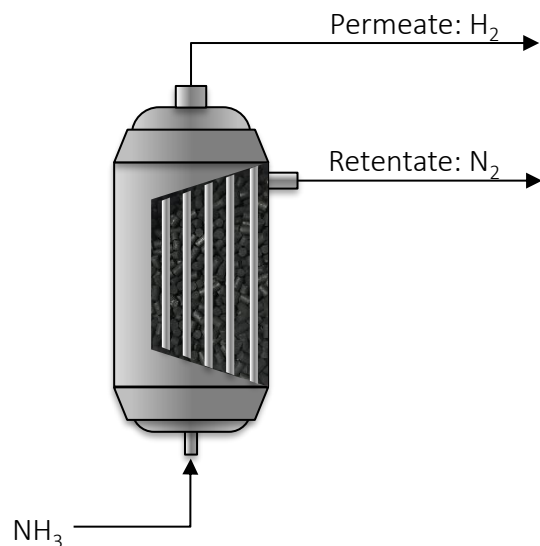


### Conventional system



### Novel technology





### Experimental conditions

$\Delta P$ [bar]	3
Permeate pressure [bar]	0.01-1
Feed flow rate [ $L_N/min$ ]	0.5
Membrane	Double-skinned Pd-Ag
Thickness selective layer [ $\mu m$ ]	~4.6 l

Compared to conventional systems, in a membrane reactor:

- ☐ Comparable or higher  $NH_3$  conversion can be achieved at lower temperature (higher efficiencies)
- ☐ High-purity  $H_2$  is recovered

*Is the membrane reactor-based system economically competitive compared to a conventional system?*

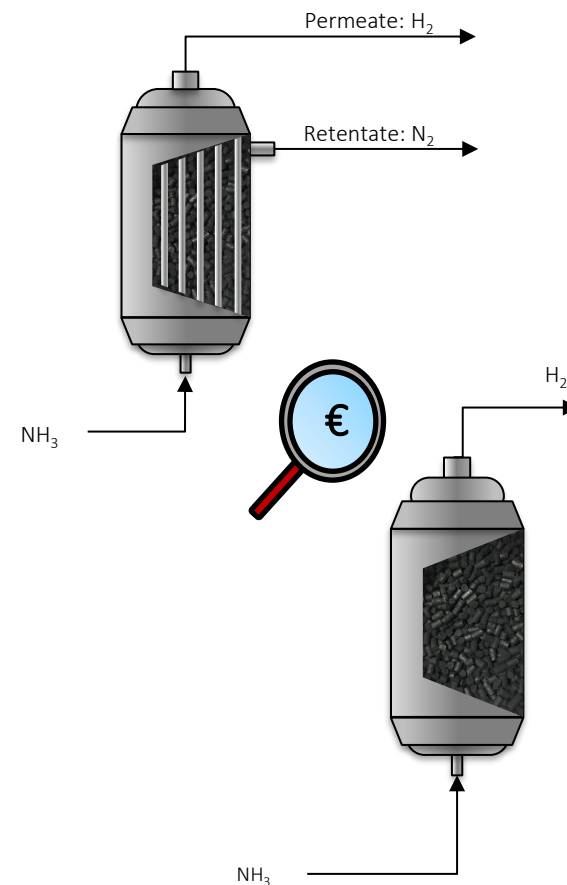


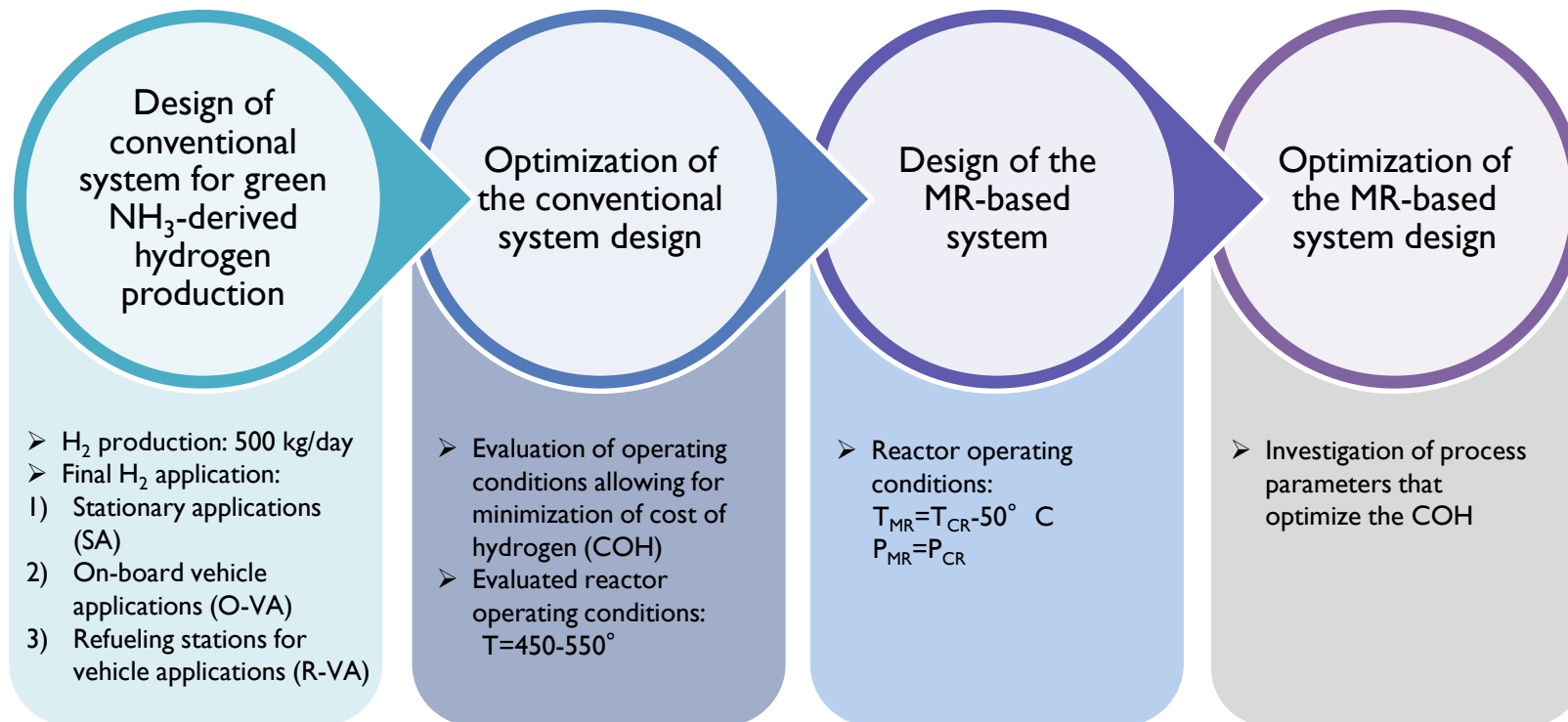
- Studies available in literature calculated the costs of hydrogen production, but a comparative study addressing a techno-economic assessment at different plant capacities and system configurations is not available.



Techno-economic assessment of a decentralized plant for hydrogen production from ammonia decomposition

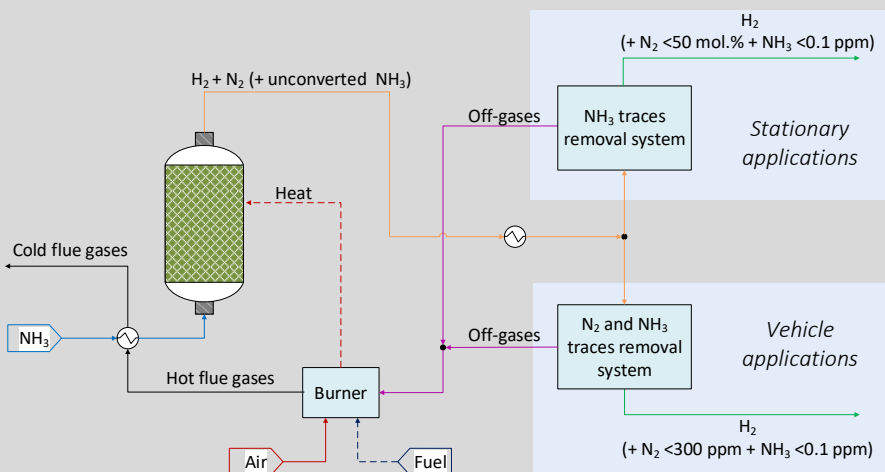
- $H_2$  for direct use in PEM fuel cells
- Applications: stationary applications (a), on-board vehicle applications (b), and refuelling stations (c)



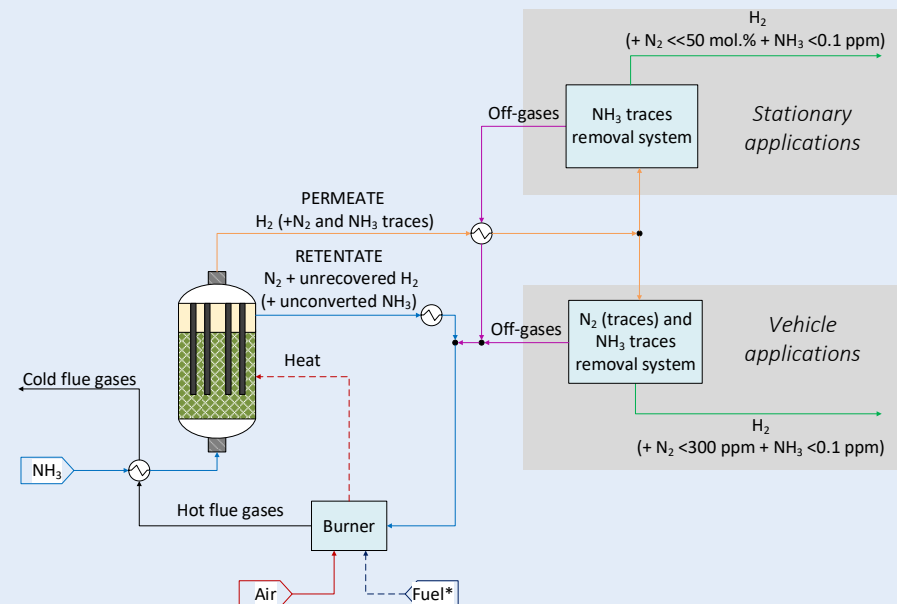


## H<sub>2</sub> production from NH<sub>3</sub>: the conventional and the MR-based systems

### Conventional system



### Membrane reactor-based system



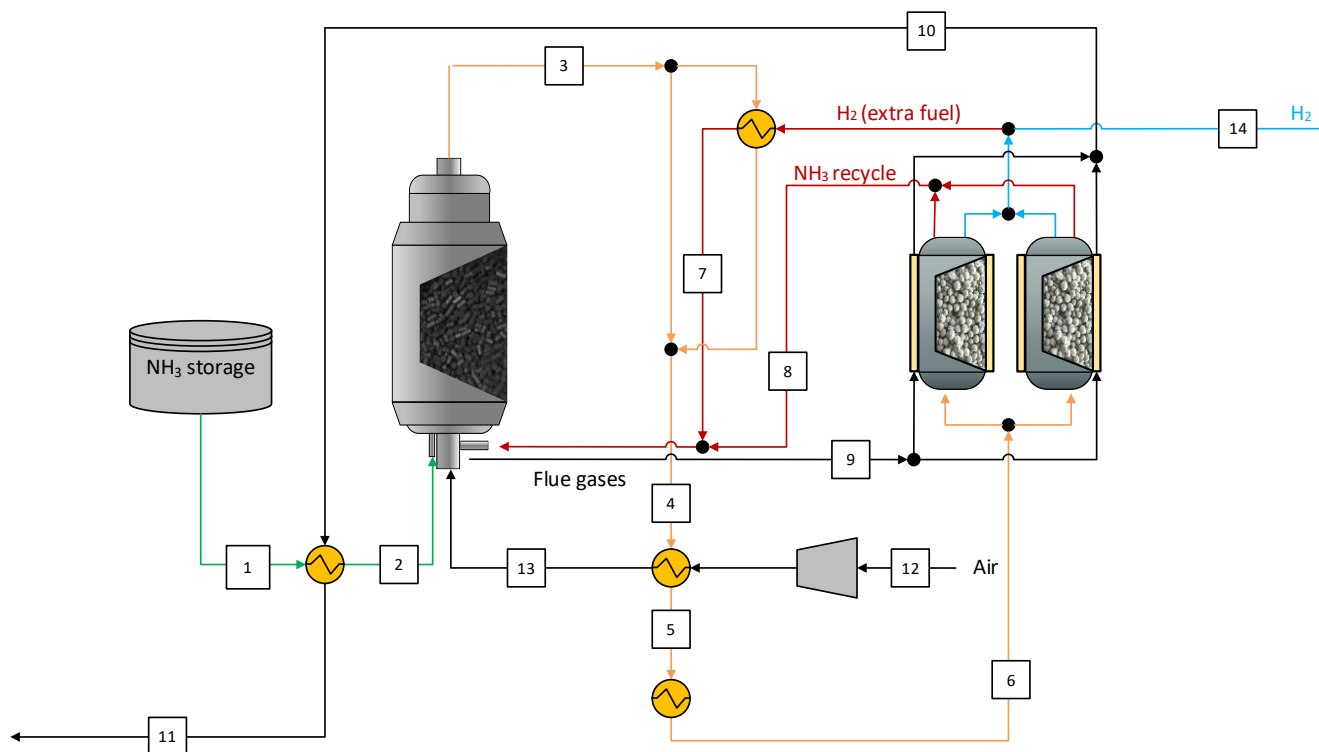
#### Target:

- 500 kg/day of H<sub>2</sub>
- H<sub>2</sub> purity = 99.97%
- Max NH<sub>3</sub> concentration in H<sub>2</sub> stream = 0.1 ppm

#### Design choices:

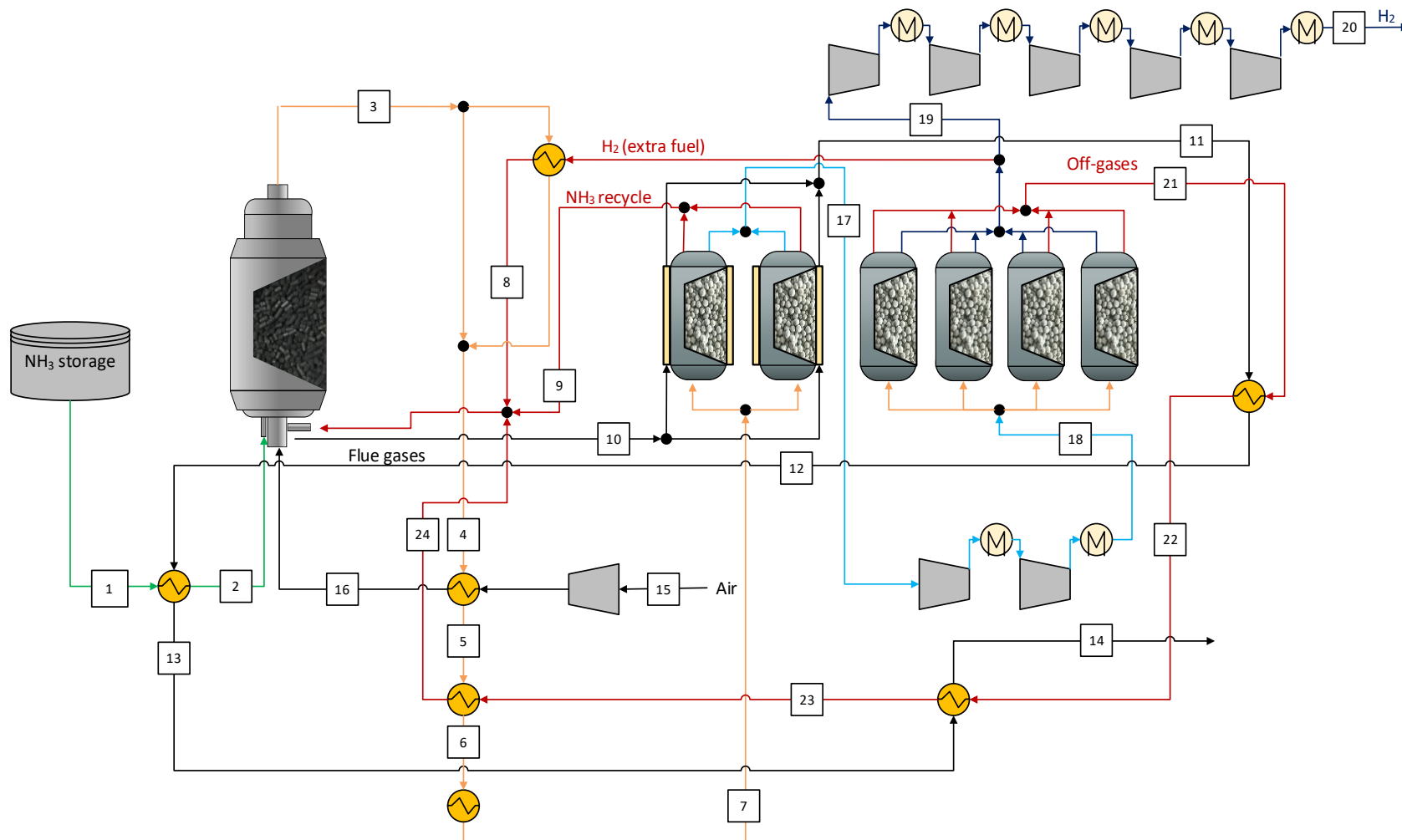
- Catalyst: Ru/Al<sub>2</sub>O<sub>3</sub>
- NH<sub>3</sub> removal unit: TSA (2 beds configuration)
- N<sub>2</sub> removal unit: PSA (4 beds configuration)

### Design of the conventional process for SA



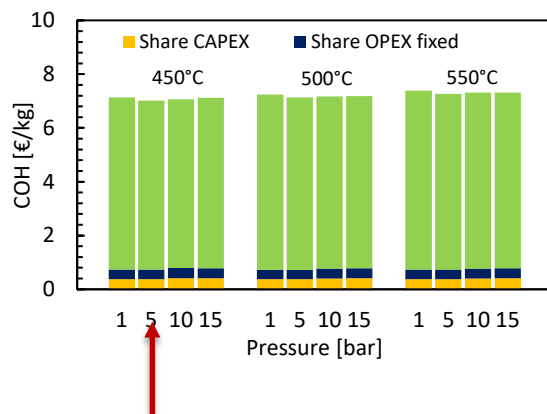


### Design of the conventional process for VA

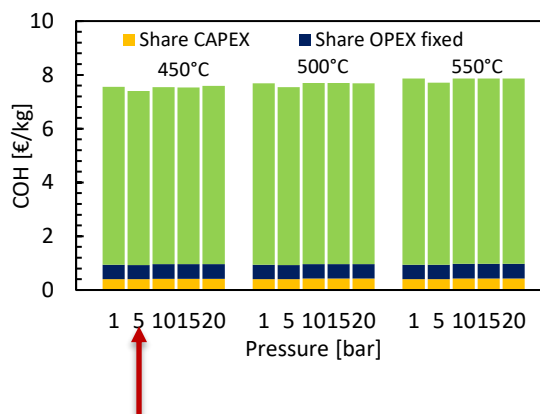


### Optimization of the conventional system

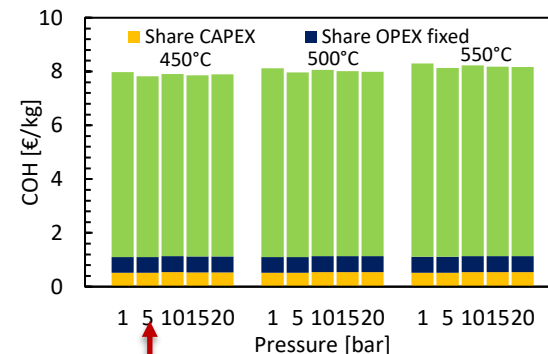
Stationary applications (SA)



On-board vehicle applications (O-VA)

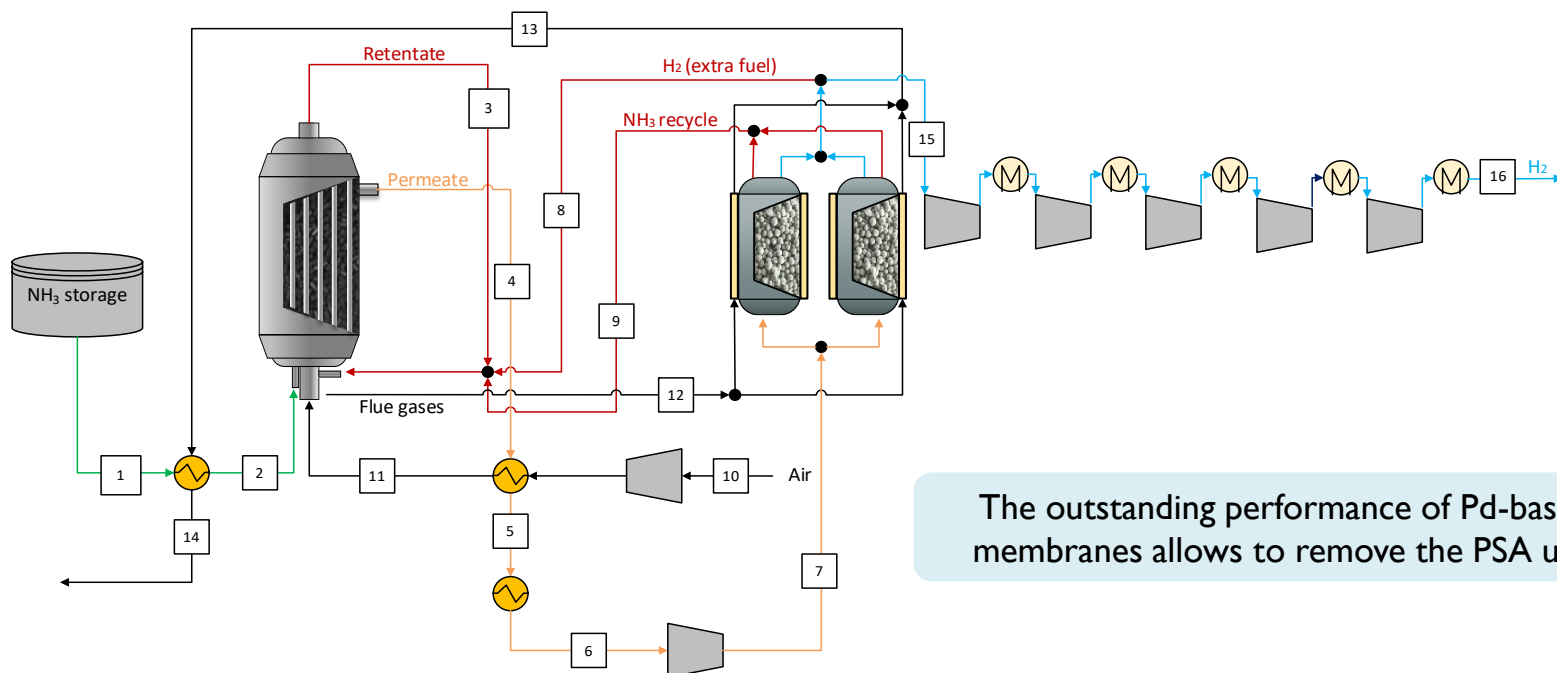


Refueling stations for vehicle applications (R-VA)

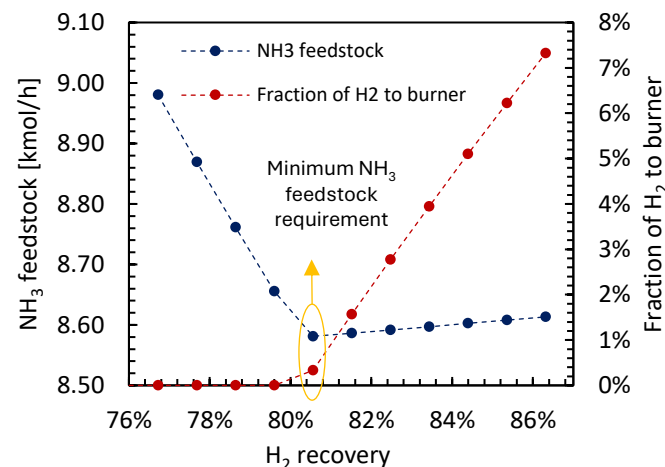
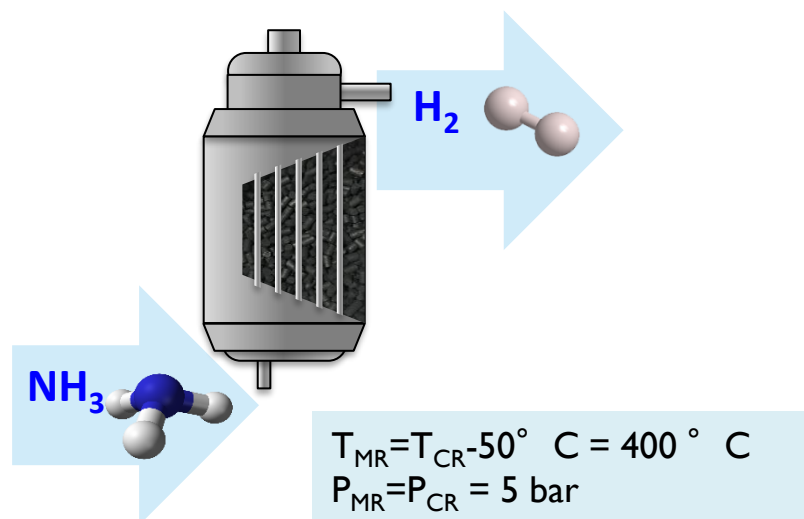


- COH in the conventional system is minimized with the reactor operated at  $T=450^{\circ}\text{C}$  and 5 bar
- The process is OPEX-intensive with the cost of the  $\text{NH}_3$  feedstock being the main contributor to COH

### Design of the MR-assisted process for SA/VA



### Optimization of MR-based system



Reactor optimization  $\neq$  Process optimization

The cost of NH<sub>3</sub> feedstock is the main contributor to COH



**Objective**

Minimization of the NH<sub>3</sub> feedstock

A higher recovery reduces the available heat from the combustion of the retentate, which leads to an increased quantity of fuel that must be burned to sustain the NH<sub>3</sub> decomposition reaction and that, in turn, implies a greater flow rate of NH<sub>3</sub> to be processed.

### Technical assessment

Process	Conventional			MR-assisted	
Application	Stationary	Vehicle on-board	Vehicle refueling stations	Stationary and vehicle on-board	Vehicle refueling stations
<b>Feedstock</b>					
NH <sub>3</sub> [kg/h]	151.03	153.46	153.46	146.15	146.15
Thermal input [kW <sub>LHV</sub> ]	780.50	793.09	793.09	755.27	755.27
<b>Chemical products</b>					
H <sub>2</sub> [kg/h]	20.83	20.83	20.83	20.83	20.83
Thermal output [kW <sub>LHV</sub> ]	693.92	693.92	693.92	693.92	693.92
<b>Cold Gas Efficiency (CGE)</b>	<b>88.91%</b>	<b>87.50%</b>	<b>87.50%</b>	<b>91.88%</b>	<b>91.88%</b>
<b>Electricity</b>					
Air blower [kW <sub>el</sub> ]	1.95	2.29	2.29	1.87	1.87
Hydrogen booster [kW <sub>el</sub> ]	-	-	28.33	19.33	37.09
Hydrogen compressor [kW <sub>el</sub> ]	-	-	46.04	-	45.85
Vacuum pump [kW <sub>el</sub> ]	-	-	-	29.69	29.69
Total electricity [kW <sub>el</sub> ]	1.95	2.29	76.74	50.89	114.50
<b>Overall plant efficiency (η<sub>tot</sub>)</b>	<b>88.69%</b>	<b>87.24%</b>	<b>79.78%</b>	<b>86.08%</b>	<b>79.78%</b>

$$CGE = \frac{\dot{m}_{H_2} LHV_{H_2}}{\dot{m}_{NH_3} LHV_{NH_3}}$$

$$\eta_{tot} = \frac{\dot{m}_{H_2} LHV_{H_2}}{\dot{m}_{NH_3} LHV_{NH_3} + \frac{Q_{el}}{\eta_{el,ref}}}$$

## Economic assessment



Is the packed bed MR technology competitive compared to the packed bed conventional technology?

### Scenario 1: stationary applications

Both in the conventional and in the MR-based systems the COH is 6.95 €/kg

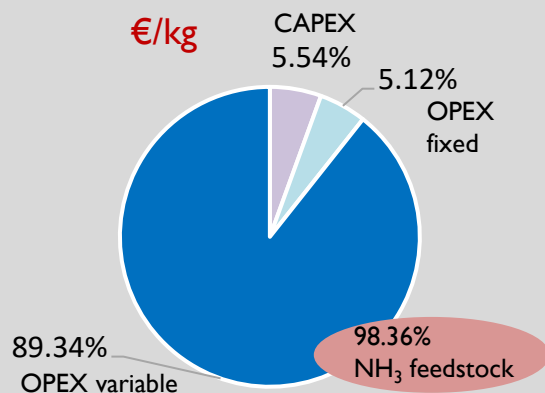
No economic advantage from utilization of the packed bed MR technology

### Scenario 2.1: on-board vehicle applications

#### Conventional system

COH = 7.15

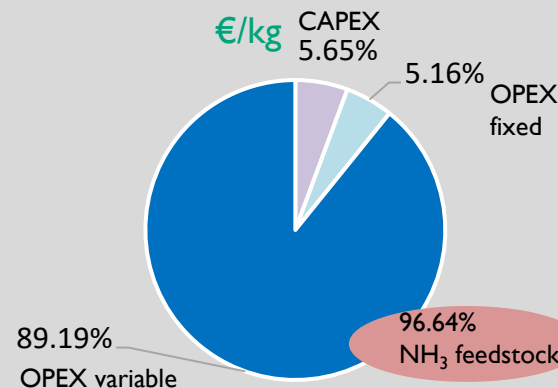
€/kg



#### MR-assisted system

COH = 6.95

€/kg

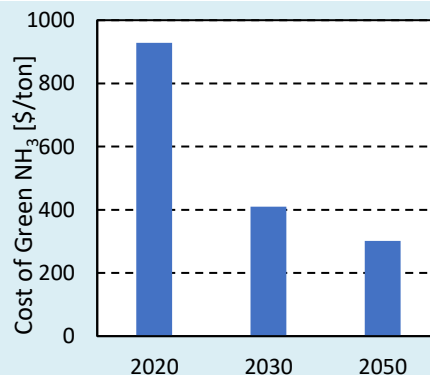
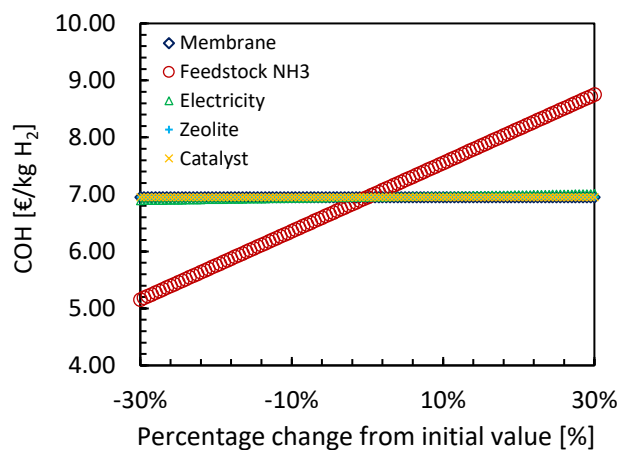


### Scenario 2.2: refueling stations for vehicle applications

Similar conclusions to scenario 2.1 with  $\text{COH}_{\text{conventional}} = 7.57 \text{ €/kg}$  and  $\text{COH}_{\text{MR-assisted}} = 7.38 \text{ €/kg}$

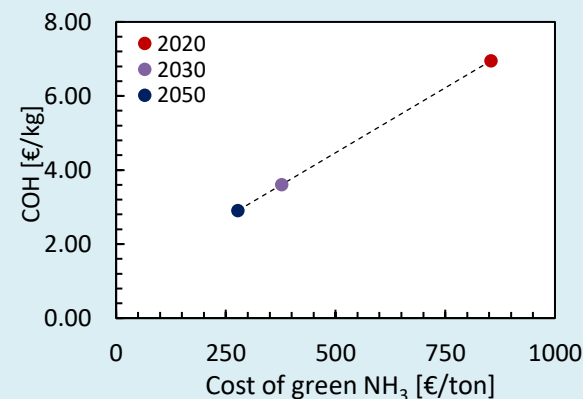
## Economic assessment

### Sensitivity analysis and forecasting



<https://www.iea.org/reports/global-hydrogen-review-2021/executive-summary>

Year	Cost of NH <sub>3</sub> [€/ton]	COH [€/kg]
2020	853.92	6.95
2030	377.07	3.60
2050	277.30	2.90



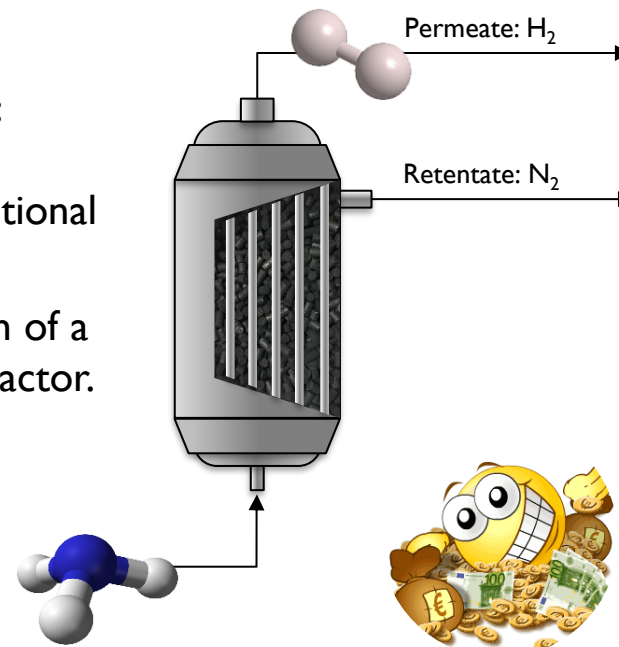


## Conclusions

### In a membrane reactor for $H_2$ production from $NH_3$ :

- ☐ Higher efficiency and compactness compared to a conventional system are achieved
- ☐ Fuel cell-grade  $H_2$  production is possible with the addition of a relatively inexpensive sorption unit downstream of the reactor.

From an economic point of view, the recovery of  $H_2$  from green  $NH_3$  using MRs can be achieved at lower costs compared to the benchmark technology.



The MR technology holds significant potential in advancing the decarbonization of the current energy system.

# Advanced materials and Reactors for Energy storage tHrough Ammonia



areNH<sub>3</sub>a

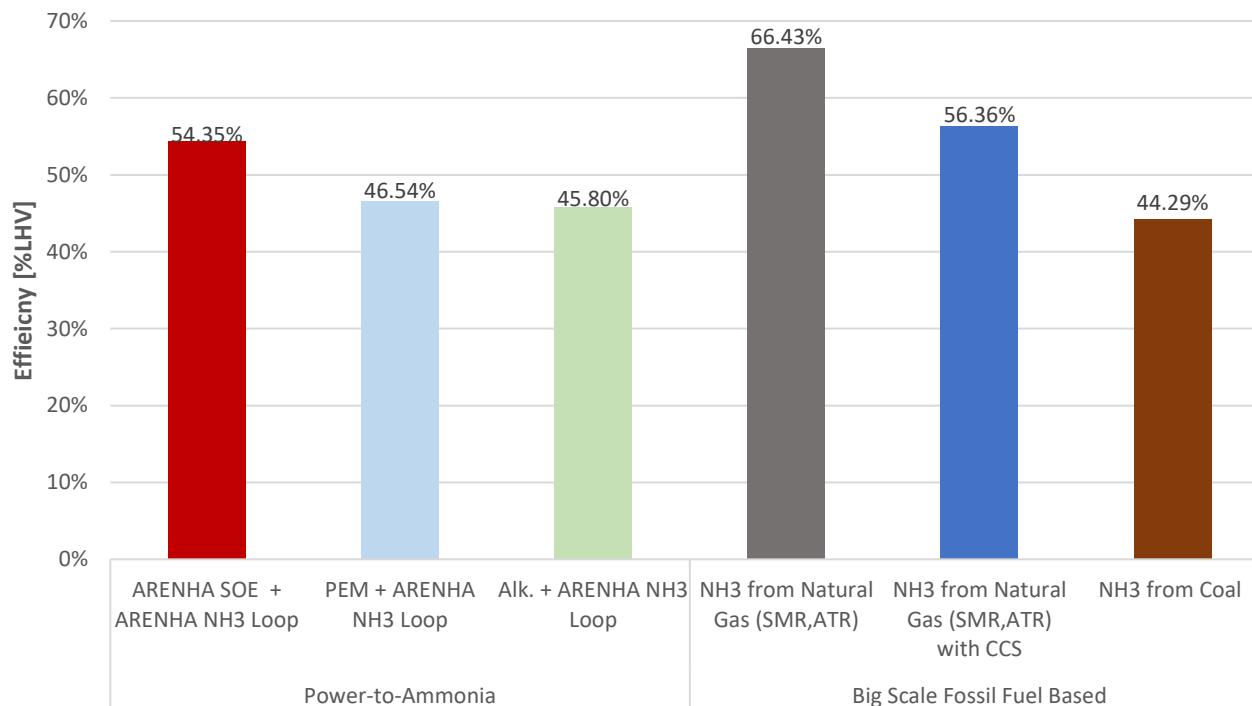
*Thank you for your attention*

Website: [arenha.eu/](https://arenha.eu/)

LinkedIn: ARENHA Project

Twitter: @ARENHA\_H2020

## Backup Slide: Power-to-Ammonia System Efficiency



## 2.6-6.4 Modelling of the Complete System and techno-economic analysis



**Economic assessment: Cost estimation methodology and reference operation parameters and economic assumptions**

$$LCOH = \frac{(TASC_{SOE} \cdot CRF) + C_{O\&M, fixed, SOE} + C_{O\&M, variable, SOE}}{M_{H2, produced}}$$

$$LCOA = \frac{(TASC_{PtA} \cdot CRF) + C_{O\&M, fixed, SOE} + C_{O\&M, variable, PtA}}{M_{NH3, produced}}$$

Cost Estimation (AACE Class IV)	
<b>Bare Erected Cost [k€]</b>	
Equipment 1 Bare Erected Cost	A
Equipment 2 Bare Erected Cost	B
Equipment n Bare Erected Cost	N
Bare Erected Cost [BEC]	A+B+...+N
<b>Direct Cost [k€]</b>	
SOEC Stack Installation	10%BEC_SOEC
EPC	15%BEC
<b>Contingencies and Owner's Cost [k€]</b>	
Project Contingencies (PC)	15%BEC
Process Contingencies (PSC)	10%(BEC+EPC+PC)
Owner's Cost (OC)	20%(BEC+EPC+PC+PSC)
<b>Total Plant Cost</b>	
Total Plant Cost (TASC)	1.1*(BEC+EPC+PC+PSC+OC)

Economic Assumptions	
Plant Operation (n)	30 years
Discount rate	7%
SOEC Stack Cost [€/kW]	300 (IKTS) – 500 (Elcogen)
SOEC Stack Installation Factor [€/kW]	40

Cost Fixed O&M	
Maintenance (SOE) [€/kg/d]	130
Maintenance (Others)	3%TOC

Cost Variable OPEX	
Electricity	50 €/MWh
Absorbent Cost	0.9 €/kg
Catalyst Cost	30 €/kg
Utilities (Refrigerant 5°C)	3.57 €/GJ
Process Water	0.23 €/m3

Electrolyser Operation		
Cell Technology	CSC (Elcogen)	
Nominal Temperature [°C]	680	800
Cell Current Density [A/cm2]	0.50	0.6
Cell Voltage [V]	~1.32	~1.29
Reactant Utilisation	70%	75%
Module Size [kW]	~530	~520
Stack Lifetime [hours]	40000	40000

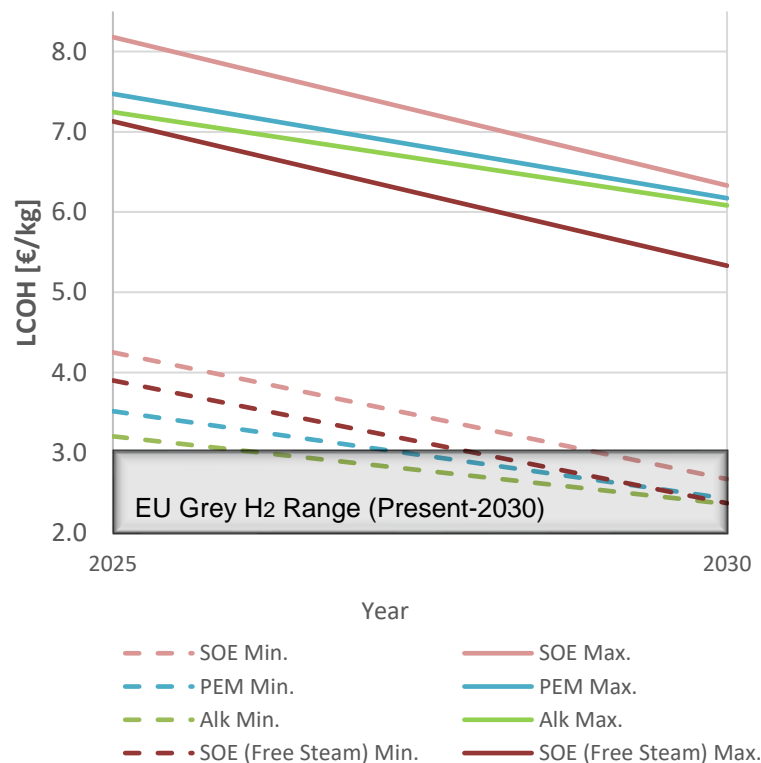
PSA Operation	
Energy Consumption	0.6 GJ/ton

H2 Storage Operation	
Nominal Pressure	100 bar

Ammonia Synthesis Loop Operation	
Nominal Reactor Pressure	80 bar
Reactor Inlet Temperature	300 °C
Catalyst Type	Fe-Based (Wu)
Absorbent Type	36% MnCl2 – 64% Silica Gel

NH3 Storage	
Storage Capacity	30 Days

## Backup Slide: Detailed assumption of electrolysis scenario analysis



Electrolyzers operated with 60% year average capacity factor. Min and Max. refer respectively to 25 and 100 €/MWh electricity cost scenario. 30 years plant lifetime and 7% WACC assumed. PEM and Alk. stack degradation [1]. PEM Alk and SOEC O&M from [1]. PEM and Alk. CAPEX and stack cost from STEPS scenario in [2]. 2025 PEM system energy consumption from [3], 2025 Alkaline system energy consumption from [4]. 2030 System energy consumption scenarios from [1].

- [1]. [Clean Hydrogen JU - SRIA Key Performance Indicators \(KPIs\) - Clean Hydrogen Partnership](#)
- [2]. IEA, Global Hydrogen Review, 2024
- [3]. Cummins Hylizer specsheet, 2021
- [4]. Sunfire-Hylink Alkaline specsheet, 2025

Scenario	2025				2030			
Electrolysis Technology	Alk	PEM	SOE	SOE (free steam)	Alk	PEM	SOE	SOE (free steam)
Installed Electrolysis Power [MW]	24.2	23.7	15.9	15.9	140	140	100	100
Hydrogen Production [t/d]	11.15				70.00			
Tot. CAPEX* [€/kW] [2]	2000	2450	4020	3921	1250	1400	2052	1980
Stack Lifetime [khr]	80	50	40		80	80	40	
O&M [€/kg/d*y] [1]	43	30	130		35	21	45	
Stack Replacement Cost [€/kW]	195	255	300		130	170	100	
<b>System Energy Consumption [kWh/kg<sub>H2</sub>]</b>	<b>52</b>	<b>51</b>	<b>49.85</b>	<b>41.10</b>	<b>48</b>	<b>48</b>	<b>47.85</b>	<b>39.10</b>

\*CAPEX is calculated per kW of installed electrolysis power: Stack energy consumption for Alk. and PEM assumed close to total system energy consumption.

**O&M:** Operation and Maintenance | **Alk:** Alkaline electrolyser | **PEM:** Proton exchange membrane electrolyzer | **SOE:** Solid Oxide Electrolyzer

**Despite higher cost greater efficiency makes SOE potentially competitive with low-T electrolysis technologies (especially with high electricity prices!)**

$$COH = \frac{(TOC \cdot CCF) + C_{O\&M, fixed} + C_{O\&M, variable}}{Capacity \cdot Plant\ availability}$$

Plant Component	Cost [k€]
Component W	A
Component X	B
Component Y	C
Component Z	D
Bare Erected Cost [BEC]	A+B+C+D
<u>Direct costs as percentage of BEC</u>	
Total Installation Costs [TIC]	80% BEC
Total Direct Plant Cost [TDPC]	BEC+TIC
Indirect Costs [IC]	14% TDPC
<b>Engineering procurement and construction [EPC]</b>	TDPC+IC
<u>Contingencies and owner's costs</u>	
Contingency	10% EPC
Owner's cost	5% EPC
<b>Total contingencies &amp; OC [C&amp;OC]</b>	15% EPC
Total Overnight Cost [TOC]	EPC+C&OC

$$C_i = C_0 \cdot \left(\frac{S_i}{S_0}\right)^n \cdot F_p \cdot F_m \cdot F_T \cdot \frac{CEPCI}{CEPCI_{reference\ year}}$$

Cost O&M fixed	
Maintenance	2.5% TOC
Insurance	2% TOC
Labor	27991 €/year/pp <sup>1</sup>

COST O&M variable	
Green NH <sub>3</sub>	853.92 €/ton <sup>2</sup>
Electricity	0.085 €/kWh <sup>3</sup>
Catalyst	143 €/kg <sup>3</sup>
Zeolite 13X	43.7 €/kg <sup>4</sup>
Membrane	6000 €/m <sup>3</sup>

Assumptions	
Plant availability	90%
Plant lifetime (n)	25 years <sup>3</sup>
Catalyst lifetime	5 years <sup>3</sup>
Lifetime Zeolite 13X	5 years
Membrane lifetime	5 years
Discount factor (i)	8% <sup>3</sup>

$$CCF = \frac{(i + 1)^n}{((i + 1)^n - 1)}$$

<sup>1</sup> [https://www.payscale.com/research/NL/Job=Chemical\\_Process\\_Operator/Salary](https://www.payscale.com/research/NL/Job=Chemical_Process_Operator/Salary)

<sup>2</sup> <https://www.iea.org/reports/global-hydrogen-review-2021/executive-summary>

<sup>3</sup> S. Richard, A. Ramirez Santos, and F. Gallucci, "PEM genset using membrane reactors technologies An economic comparison among different e-fuels", International Journal of Hydrogen Energy

<sup>4</sup> <https://www.msесupplies.com/products/1kg-molecular-sieves-13x-pellets-spheres?variant=31758805205050>

### Technical assessment

	Conventional process Stationary applications	Conventional process Vehicle applications	MR-assisted process Stationary and vehicle applications
<b>Reactor operating conditions</b>			
Reaction temperature [°C]	450	450	400
Reaction pressure [bar]	5	5	5
Permeate pressure [bar]	-	-	0.1
<b>Feedstock</b>			
NH <sub>3</sub> flow rate at reactor inlet	151.03 kg/h 8.87 kmol/h	153.46 kg/h 9.01 kmol/h	146.15 kg/h 8.58 kmol/h
<b>Energy requirement</b>			
Thermal input [kW]	127.51	129.58	123.72
<b>KPI</b>			
NH <sub>3</sub> conversion	97.8%	97.8%	99.1%
H <sub>2</sub> recovery	-	-	80.6%
Reactor efficiency ( $\eta_{\text{reactor}}$ )	96.2%	96.2%	79.2%* (97.4%**)
$\eta_{\text{NH}_3 \text{ to H}_2}$	5.8 kg/kg	5.8 kg/kg	7.0 kg/kg* (5.7 kg/kg**)

\* Calculated considering as valuable reaction product only hydrogen available at the reactor's permeate side

\*\* Calculated considering as valuable reaction product both the hydrogen available at the reactor's permeate and retentate sides

$$\eta_{\text{reactor}} = \frac{\dot{m}_{\text{H}_2} \text{LHV}_{\text{H}_2}}{\dot{m}_{\text{NH}_3} \text{LHV}_{\text{NH}_3} + W_{\text{in}}}$$